

The significance of the mineralogical and surface characteristics of gold grains in the recovery process

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SYNOPSIS

A description is given of the nature and occurrence of gold at various stages in the process of its recovery from Witwatersrand and related ores. Electron microprobe investigations show that the surface of gold grains in the ore is already coated. During metallurgical processing, further coatings, mainly hydrated iron oxides, accumulate on the grains. Theories are advanced for the formation of these coatings, and the adverse effects on metallurgical operations are discussed.

SINOPSIS

'n Beskrywing word gegee van die aard en voorkoms van goud op verskeie stadiums in die prosesse van herwinning van Witwatersrand en verwante ertsse. Elektronemikrobuis ondersoek het aan die lig gebring dat die oppervlakte van goud greintjies in die erts reeds aangepak is. Gedurende metallurgiese bewerking versamel meer aanpaksels, veral gehidreerde ysterhidroksiede, op die greintjies. Teorieë vir die ontwikkeling van hierdie aanpaksels word voorgelê en die ongunstige invloed op metallurgiese prosesse word bespreek.

INTRODUCTION

Several suites of plant products and numerous individual samples were received from Anglo American Corporation gold mines, notably Western Deep Levels, the Vaal Reefs mines, Western Holdings, and Trekkies. These samples were examined in an attempt to find out more about the degree of liberation of the gold, its mode of occurrence and associations, size distribution, and other features that could influence the efficiency of gold recovery.

A number of reef samples were also studied in detail to obtain information on the characteristics of the original gold particles before their exposure to plant conditions.

Heavy concentrates were prepared from the various plant products, and these, together with the light fractions, were examined by optical microscopy and other mineralogical techniques supplemented where necessary by electron-microprobe analysis of selected grains. The relative abundance of the various kinds of gold-bearing grains present in the samples was expressed in terms of mass percentages, the masses being calculated from the sizes of the gold particles. It must be stressed that, owing to the comparatively small number of gold grains exposed in most of the polished sections, the results are approximate and give

only a rough indication of the relative amounts.

Gold particles that, although attached to or partially occluded by gangue constituents, are sufficiently exposed to permit ready dissolution (or amalgamation) are, for the present purpose, classified as "free gold" — see, for example, photomicrograph 1, Plate 1.

RESIDUES

In an investigation of this nature the most logical place to start is at the tail-end of the plant — the residue dumps. A knowledge of the appearance and mode of occurrence of the gold still present in residues could well provide important clues to why this gold had not been recovered in the plant.

We have studied residue samples from several localities and have found that certain features are common to all.

One of the main gold carriers in all residue samples (in calcine leach residues, frequently the only gold carrier) is thucholite, that enigmatic hydrocarbon loaded with occlusions of uraninite and, usually, gold. Total precious metals assays on the thucholite concentrates we have prepared gave values ranging from a few hundred to several thousand grams per tonne.

Thucholite is not concentrated in the plant, nor is much of its load of occluded gold released on calcining during sulphuric acid manufacture, as practised in the Group. In thucholite, the property of light-

ness is combined with extreme refractoriness, and it is not surprising that this constituent is such a common cause of losses in gold-plant residues.

The problem of recovering and treating thucholite is still being examined, and in this paper only casual reference will be made to this important material.

Apart from thucholite, sulphide grains occurring in residue samples were seen to occlude small specks or veinlets of gold. More rarely, gold occlusions were noted in quartz, in poorly preserved uraninite, skutterudite, leucoxene, limonitic material, and a variety of other gangue constituents.

An occasional grain of free gold was seen in most of the residue samples, and, in spite of its scarcity, this form of gold usually accounts for almost the entire gold content of the sample (excluding gold associated with thucholite), as reference to Table 1 will show. These grains range in size from less than 0.075 mm to over 0.075 mm, and the majority have the following features in common:

- (i) The grains are enveloped in a distinct coating of hydrated iron oxide.
- (ii) The grains are frequently flattened or otherwise distorted, and extraneous mineral matter may have been pressed into the grains.

It is understandable that small specks of gold occluded in gangue

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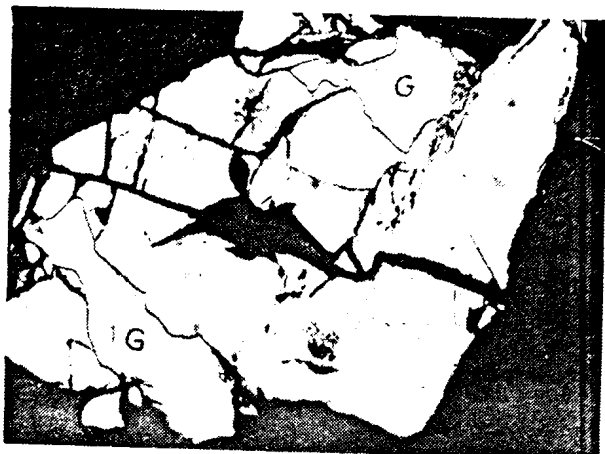


PLATE I

Photomicrographs

1	2
3	4
5	6

Photomicrograph 1

Fractured aggregate of pyrite (grey) and gold (white). In spite of the gold being attached to pyrite and partly occluded by it, it is sufficiently exposed

Description of Photomicrographs

for ready dissolution. Freddie's: Minus 3/4" Dry crusher product. X 620.

Photomicrograph 2

Distorted gold grain (G). Western Holdings: Feed to Cleaner Tables Nos. 1 and 2 banks. X 600.

Photomicrograph 3

Flattened gold grain (G). The flake is intersected at right angles by the surface of the polished section. Freddie's: Secondary cyclone underflow. X 620.

Photomicrograph 4

Partially amalgamated gold. The porous zone of the grain is pale in appearance, the colour gradually deepening to normal golden yellow towards the solid, unamalgamated portion. Western Holdings: Johnson Concentrator Tails No. 3 Bank. X 600.

Photomicrograph 5

Gold grain enveloped in transparent amorphous material. Western Holdings: Mine Sludge. X 600.

Photomicrograph 6

Gold (white) encrusted by hydrated iron oxide (grey). Sallies Dump. X 600.

constituents may find the residue, but the loss of gold is probably due to heavy tarnish on the surface of the gold grains. The effects of excessive washing changes the properties of the gold grains. In some of the samples, gelatinous material present of settling agent. This material may encrust the gold grains and could have prevented the dissolution of the gold grains. The question that arises is: when and how did the gold acquire the product? It prevented their recovery. Later in this paper, the problem of coating the

Designation of samples

Dry crusher product minus 3/4" from Symons screen

Crusher rake
Classifier
Underflow

Crusher rake
Classifier
Overflow

Ball mill feed

Ball mill
Cyclone
Underflow

Ball mill
Cyclone
Overflow

Tube mill
Discharge

Secondary cyclone
Underflow

Secondary cyclone
Overflow

Combined residue
Washed

Freddie's washed
residue (incompletely
dissolved)

Excluding gold locked in

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mated gold. The grain is pale in ap-
 gradually deepen-
 yellow towards
 amated portions.
 Johnson Concer-
 ank. X 600.
 d in transparent
 . Western Hold-
 600.
 uested by hydrated
 lies Dump. X 600.

constituents may find their way into
 residue, but the loss of the free
 is probably related to the
 y tarnish on the grains and to
 effects of excessive milling, which
 changes the properties of the gold
 grains. In some of the residue
 samples, gelatinous materials remini-
 ment of settling agents were seen.
 This material may envelop mineral
 grains and could conceivably have
 prevented the dissolution of some
 of the gold grains.

The question that now arises is,
 when and how did the grains of free
 gold acquire the properties that
 prevented their recovery in the
 plant? Later in this paper the mech-
 anism of coating the grains and the

plant conditions that contribute to
 the formation of a coating will be
 examined in some detail.

Also, the fact that occluded gold
 (again excluding gold associated with
 thucholite) constitutes such a very
 subordinate proportion of the gold
 in most of the residues examined
 indicates that gold has been liberated
 adequately in the plant — as a matter
 of fact, the flattened appearance of so
 many of the grains suggests gross
 over-milling.

As a next step we shall examine
 the occurrence of gold in the various
 plant products; but, before doing so,
 let us consider the gold occurring
 in the mine sludge, before it even
 reaches the plant.

MINE SLUDGE

The appearance of the sludge
 differs from mine to mine, and de-
 pends largely on the particular pro-
 cedure adopted to separate the
 sludge from the mined ore. In the
 mine sludge from Western Hold-
 ings, for example, the gold grains are
 considerably coarser grained than
 those in the Western Deep Levels
 sludges. (See Tables III and IV.) How-
 ever, there are certain significant
 features in common with all the
 sludge samples examined. These are:

- (i) Auriferous thucholite is abund-
ant.
- (ii) Almost all of the remainder of the
gold is liberated, the common
practice of drilling and blasting

TABLE I
 FREDDIES CONSOLIDATED MINES LIMITED
 SUMMARY OF MINERALOGICAL DATA

Designation of sample	Size analysis		Precious metals assay		Gold occurrence (Mass %) Free		Locked*
	μm	Wt. %	Gold	Silver	μm		
Crusher product plus 1/2" from Symons screen	+600 +150 -150	94 3 3	7,9 Insufficient Insufficient	1,7	+150 +75 -75	78 12	10
Crusher rake Classifier Underflow	+600 +150 -150	82 16 2	12,7 12,0 Insufficient	1,6 1,7	+150 +75 -75	76 16	8
Crusher rake Classifier Overflow	+600 +150 -150	<1 6 94	5,8	1,3	+150 +75 -75	83 15	2
Ball mill feed	+600 +150 -150	85 12 3	3,8 19,7 40,3	0,7 2,2 4,9	+150 +75 -75	95 5	<1
Ball mill Cyclone Underflow	+600 +150 -150	64 19 17	141,6	13,0	+150 +75 -75	53 45 2	<1
Ball mill Cyclone Overflow	+600 +150 -150	21 27 52	14,7	2,0	+150 +75 -75	79 20	1
Tube mill Discharge	+600 +150 -150	7 33 60	161,9	13,5	+150 +75 -75	53 46 1	<1
Secondary cyclone Underflow	+600 +150 -150	14 39 47	190,1	14,8	+150 +75 -75	47 48 5	<1
Secondary cyclone Overflow	+600 +150 -150	1 5 94	18,1	2,4	+150 +75 -75	62 31 6	1
Combined residue Washed	+600 +150 -150	<1 3 97	0,5	0,6	+150 +75 -75	— — 92	8
Freddies washed residue (incompletely dissolved)	+600 +150 -150	<1 4 96	0,4	0,4	+150 +75 -75	insufficient	

*Excluding gold locked in thucholite

TABLE II
VAAL REEFS WEST GOLD MINE
SUMMARY OF MINERALOGICAL DATA

Designation of sample	Size analysis		Precious metals assay		Gold occurrence (Mass %)		Locked*
	μm	Wt. %	Gold	Silver	μm	Free	
Washing plant Overflow	+150 —150	8 92	22,0 24,4	1,6 1,7	+150 +75 —75	— — 99	1
Washing plant Underflow Rake return	+150 —150	91 9	31,8 131,8	0,8 6,5	+150 +75 —75	— 78 21	1
Waste washing plant Waste sludge			18,3		+150 —150	89 11	<1
Waste washing plant Reef sludge and stock pile fines	+1 mm +300 +150 —150		1,1 1,9 5,3 6,9		+150—300 —150	88 12	<1
Low grade Primary mill discharge	+150 —150	61 39	9,2 18,3	0,8 1,5	+150 +75 —75	— — 95	5
Low grade Primary cyclone Overflow	+150 —150	55 45	9,9 17,0	0,8 1,2	+150 +75 —75	— 61 38	1
Low grade Primary cyclone Underflow	+150 —150	84 16	12,4 57,6	1,0 3,6	+150 +75 —75	— 69 30	1
Low grade Secondary tube Mill discharge	+150 —150	56 44	23,0 171,7	2,7 9,3	+150 +75 —75	17 68 15	<1
Low grade Secondary cyclone Overflow	+150 —150	18 82	3,7 8,8	0,2 0,8	+150 +75 —75	— 80 20	<1
Low grade Secondary cyclone Underflow	+150 —150	81 19	20,5 289,0	1,9 13,3	+150 +75 —75	— 78 18	4
Low grade Pulp head or Slimes original					+150 +75 —75	— 71 28	<1
Low grade Unwashed Residue					+150 +75 —75	— 74 22	4
High grade Primary mill Discharge	+150 —150	66 34	13,7 22,3	1,1 1,8	+150 +75 —75	— 89 11	<1
High grade Primary cyclone Overflow	+150 —150	57 43	7,6 15,4	0,7 1,2	+150 +75 —75	— 81 18	1
High grade Primary cyclone Underflow	+150 —150	81 19	14,5 55,2	1,0 3,2	+150 +75 —75	— 39 60	1
High grade Secondary tube Mill discharge	+150 —150	68 32	14,9 164,2	1,2 8,3	+150 +75 —75	— 65 35	<1
High grade Secondary cyclone Overflow	+150 —150	15 85	3,1 11,8	0,1 0,8	+150 +75 +75	— — 97	3
High grade Secondary cyclone Underflow	+150 —150	75 25	8,4 97,2	0,8 5,8	+150 +75 —75	— 80 20	<1
High grade Pulp head or Slimes original					+150 +75 —75	— 65 33	2
High grade Unwashed residue					+150 +75 —75	— 33 62	5
Flotation plant tails					+150 +75 —75	— 83 17	<1

Designation of sample

Sludge from
No. 3 shaft

Sludge from
No. 2 shaft

Low grade
by screening
minus 3"

Low grade
mill
feed

Low grade
cyclone classifier
Overflow

Low grade
tube mill
Discharge

Low grade
secondary
cyclone feed

Low grade
secondary cyclone
Overflow

Low grade
secondary cyclone
Underflow

Low grade
tertiary cyclone
Overflow

Low grade
tertiary cyclone
Underflow

Low grade
Johnson tails

High grade
tube mill
Discharge

High grade
secondary cyclone
feed

High grade
secondary cyclone
Overflow

High grade
secondary cyclone
Underflow

High grade
tertiary cyclone
Overflow

High grade
tertiary cyclone
Underflow

High grade
Johnson Tails

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*Excluding gold locked in thucholite

TABLE III
WESTERN DEEP LEVELS GOLD MINE
SUMMARY OF MINERALOGICAL DATA

Designation of sample	Size analysis		Precious metals assay		Gold occurrence (Mass %) Free		Locked*
	μm	Wt. %	Gold	Silver	μm		
Edge from shaft	Not determined				+150 +75 +75	— 89 11	I
Edge from shaft	Not determined				+150 +75 —75	— 69 30	I
Low grade dry screening minus 3"	+2,4 mm +1 mm +400 +200 +150 —150	56 18 11 7 3 5	2 13 10 10 12 19	21 2 1 1 2 2	+200—400 +150 —150	75 19 6	> I
Low grade ball mill feed	+2,4 mm +1 mm +400 +200 +150 —150	70 12 7 6 3 2	7 14 13 15 26 62	— 1 2 2 4 8	+200—400 +150 —150	77 20 3	> I
Low grade skins classifier Overflow	+150 —150	54 46	11	1	+150 +75 —75	66 18 15	> I
Low grade tube mill Discharge	+150 —150	30 70	41	6	+150 +75 —75	44 48 8	> I
Low grade secondary cyclone feed	+150 —150	49 51	80	9	+150 +75 —75	83 15 2	> I
Low grade secondary cyclone Overflow	+150 —150	3 97	10	2	+150 +75 —75	65 28 7	> I
Low grade secondary cyclone Underflow	+150 —150	54 46	56	7	+150 +75 —75	51 40 9	> I
Low grade tertiary cyclone Overflow	+150 —150	30 70	45	6	+150 +75 —75	53 43 4	> I
Low grade tertiary cyclone Underflow	+150 —150	43 57	80	10	+150 +75 —75	62 33 5	> I
Low grade Johnson tails	+150 —150	17 83	100	13	+150 +75 —75	23 64 13	< I
High grade tube mill Discharge	+150 —150	8 92	119	15	+150 +75 —75	77 17 6	< I
High grade secondary cyclone feed	+150 —150	32 68	60	7	+150 +75 —75	66 28 6	< I
High grade secondary cyclone Overflow	+150 —150	— 100	27	4	+150 +75 —75	55 28 17	< I
High grade secondary cyclone Underflow	+150 —150	33 77	143	18	+150 +75 —75	32 50 17	< I
High grade tertiary cyclone Overflow	+150 —150	4 96	58	8	+150 +75 —75	38 35 27	< I
High grade tertiary cyclone Underflow	+150 —150	31 69	240	34	+150 +75 —75	43 40 16	I
High grade Johnson Tails	+150 —150	29 71	334	42	+150 +75 —75	57 31 12	< I

TABLE III (Continued)

Designation of sample	Size analysis		Precious metals assay		Gold occurrence (Mass %)		Locked
	μm	Wt. %	Gold	Silver	μm	Free	
Belt concentrator Feed	+150 —150	41 59	2 324	269	+150 + 75 — 75	52 38 10	1
Belt concentrates	+150 —150	25 75	75**	9**	+150 + 75 — 75	53 35 12	<1
Belt tails	+150 —150	31 69	1 293	216	+150 + 75 — 75	53 35 12	<1

*Excluding gold locked in thucholite

**Kg/tonne

TABLE IV
WESTERN HOLDINGS
SUMMARY OF MINERALOGICAL DATA

Designation of sample	Size analysis		Precious metals assay		Gold occurrence (Mass %)		Locked
	μm	Wt. %	Gold	Silver	μm	Free	
Mine sludge	Not determined				+200 +150 + 75 — 75	41 27 31 1	<1
No's 1 and 2 Shaft sludge	+300 +150 + 75 — 75	1 23 53 23	18,0		+150 + 75 — 75	Inadequate Sample	
No. 3 shaft sludge	+300 +150 + 75 — 75	1 34 41 24	9,0		+150 + 75 — 75	Inadequate Sample	
Composite rake Classifier overflow	+300 +150 + 75 — 75	4 25 34 37	41,8		+150 + 75 — 75	64 25 10	1
Composite rake Classifier return	+6 mm +3 mm +300 +150 + 75 — 75	4 40 44 9 2 1	41,2		+150—300 + 75 — 75	80 15 2	3
Composite washing Plant cyclone Underflow	+300 +150 + 75 — 75	35 42 16 7	63,0		+150 + 75 — 75	67 23 7	3
Composite dewatering Cyclone underflow	+300 +150 + 75 — 75	18 37 31 14	350,3		+150 + 75 — 75	48 43 7	2
Composite ball Mill feed	+13 mm +6 mm +3 mm +300 +150 + 75 — 75	3 18 29 40	21,3		+150—300 + 75 — 75	68 28 2	2
Composite ball mill Cyclone overflow	+300 +150 + 75 — 75	28 24 18 30	17,7		+150 + 75 — 75	66 24 2	8
Composite secondary Tube outlet	+300 +150 + 75 — 75	2 21 45 32	50,2		+150 + 75 — 75	— — 99	1
Composite secondary Cyclone underflow	+300 +150 + 75 — 75	19 34 38 9	52,1		+150 + 75 — 75	46 45 9	<1

Designation of sample

Composite kreb
secondary cyclone
underflowComposite tertiary
tube outletComposite tertiary
cyclone overflowComposite Johnson
concentrator tails No. 1 and 2
bankComposite Johnson
concentrator tails No. 3
bankComposite feed to
cleaner tables Nos.
1 and 2 banks

Composite feed to No. 3 cleaner

Composite cleaner
table tailings Nos.
1 and 2 banksComposite cleaner
table tailings No. 3
bank

*Excluding gold locked in thucholite

in the reef probably due to the ready liberation of metal (see Tables I and II). Most of the gold particles readily show a thin coating, and on some grains this coating is a few it may even be as heavy. Photomicrograph Plate II depicts a grain surrounded by hydroxide, probably deposited as a suspension of colloidal materials.

Particles of rusty trachite are common, and most of them constitute the main part of the secondary iron coating the gold. The bulk of the secondary iron oxide in the sludge is as fragments of malachite in form or banded deposits.

ence
(%) Free Locked

52 } 38 } 10 }	1
53 } 35 } 12 }	1
53 } 35 } 12 }	1

41 } 27 } 31 } 1 }	< 1
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Inadequate Sample

Inadequate Sample

64 } 25 } 10 }	1
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80 } 15 } 2 }	3
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67 } 23 } 7 }	3
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48 } 43 } 7 }	2
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68 } 28 } 2 }	2
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66 } 24 } 2 }	8
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— } 99 }	1
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46 } 45 } 9 }	< 1
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TABLE IV (Continued)

Designation of sample	Size analysis		Precious metals assay		Gold occurrence (Mass %)		Locked*
	μm	Wt. %	Gold	Silver	μm	Free	
Composite kreb secondary cyclone overflow	+300 +150 +75 -75	17 32 35 16	426,4		+150 +75 -75	47 39 13	1
Composite tertiary circuit outlet	+300 +150 +75 -75	3 24 39 34	349,8		+150 +75 -75	70 22 7	1
Composite tertiary circuit overflow	+300 +150 +75 -75	2 21 45 32	40,6		+150 +75 -75	41 47 7	5
Composite Johnson concentrator tails No. 1 and 2	+300 +150 +75 -75	10 35 36 19	212,5		+150 +75 -75	76 22 2	< 1
Composite Johnson concentrator tails No. 3	+300 +150 +75 -75	8 34 33 25	179,5		+150 +75 -75	24 67 9	< 1
Composite feed to cleaner tables Nos. 1 and 2 banks	+300 +150 +75 -75	6 26 45 23	2 559,2		+150 +75 -75	58 26 5	11
Composite feed to No. 3 cleaner bank	+300 +150 +75 -75	7 25 46 22	2 862,8		+150 +75 -75	77 20 3	< 1
Composite cleaner table tailings Nos. 1 and 2 banks	+300 +150 +75 -75	6 24 49 21	1 244,9		+150 +75 -75	92 6 2	< 1
Composite cleaner table tailings No. 3	+300 +150 +75 -75	7 27 39 27	179,5		+150 +75 -75	58 40 2	< 1

*Excluding gold locked in thucholite

in the reef probably contributing to the ready liberation of the metal (see Tables III and IV). Most of the gold particles already show a thin iron oxide coating, and on some of the grains this coating is distinct. On a few it may even be described as heavy. Photomicrograph 4, Plate II depicts a grain of gold surrounded by hydrated iron oxide, probably deposited from a suspension of colloidal materials.

n) Particles of rusty tramp iron are common, and most probably constitute the main source of the secondary iron compounds coating the gold. However, the bulk of the secondary hydrated iron oxide in the sludge occurs as fragments of massive, colloform or banded deposits that do

not occlude other mineral particles, and have evidently been precipitated from a comparatively clear, colloidal suspension. In view of evidence of copious supplies of secondary, hydrated iron oxide, it appears anomalous that mineral aggregates cemented together by iron oxide are so rare in mine sludge. In the plant, such aggregates can be seen to form very readily, frequently encrusting the walls of, for example, sumps and launders, and one would expect similar deposits underground in gullies, depressions, and channels. These ferruginous aggregates are frequently very rich in gold, and the possibility of some of the metal being permanently lost underground is at present being examined.

In the sludge samples examined, the presence of materials resembling gelatinous settling agents is very much in evidence. In photomicrograph 5, Plate I, for example, a grain of gold enveloped in hardened, resinous material is illustrated. Such material must undoubtedly play an inhibiting role in the cyanidation of the gold. Mine sludges have also been found to contain various unexpected constituents, usually of no more than passing interest. Almost all of the sludges examined to date contain, sometimes in fair amounts, pulverulent or scaly zincite (ZnO) probably derived from the decomposition of galvanized materials, such as ventilation pipes.

We shall now consider the behaviour of the gold during its passage through the reduction plant.

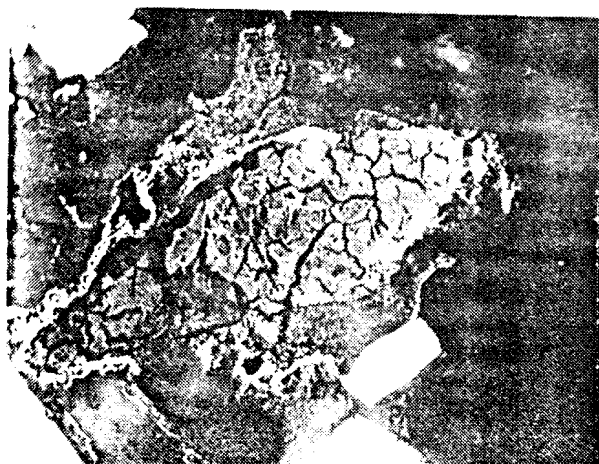
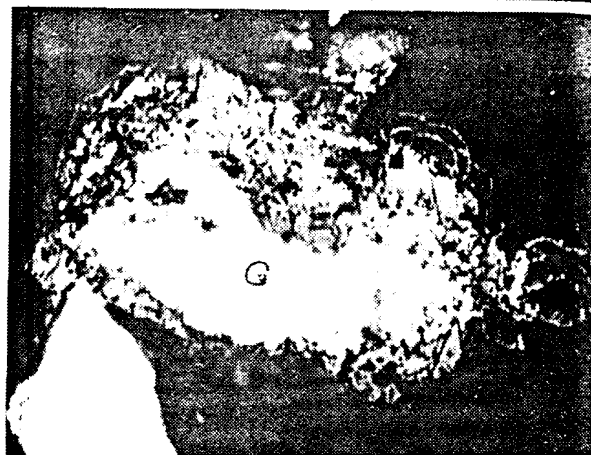
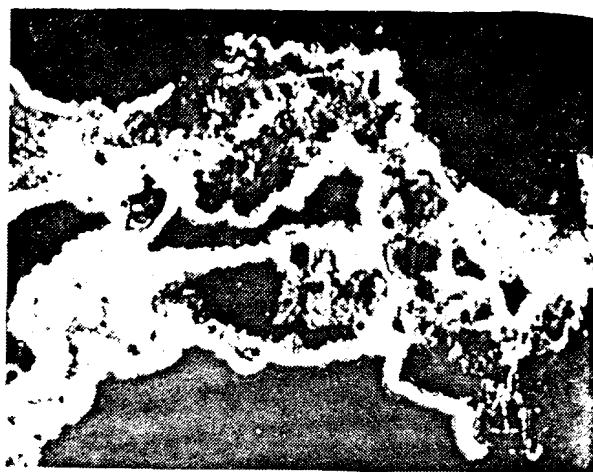


PLATE II

Photomicrographs

1	2
3	4
5	6

Photomicrograph 1

Pyrite (white) partially altered to hydrated iron oxide (dark grey). Sallies: Screening Plant Minus 1/2" Fraction. X 600.

Photomicrograph 2

Deposit of hydrated iron oxide

(white) incorporating a variety of mineral fragments (black and grey). Sallies: Screening Plant Minus 1/2" Fraction. X 600.

Photomicrograph 3

Newly formed limonitic nodule showing concentric build and typical shrinkage cracks. Sallies: Screening Plant Minus 1/2" Fraction. X 600.

Photomicrograph 4

Gold (white) encrusted by colloform hydrated iron oxide. Western Holdings: Mine Sludge. X 600.

Photomicrograph 5

Completely rusted grain of iron. Attached are grains of pyrite (white) and quartz (dark grey). Western Deep Levels: Belt feed. X 600.

Photomicrograph 6

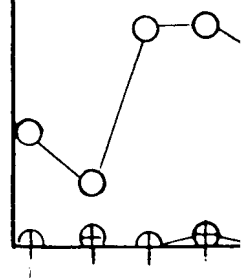
Auriferous scale. The mineral grain (mainly pyrite, gold and quartz) are cemented together by hydrated iron oxide. The ratio of gold to pyrite (both appear white on the photomicrograph) is about 1:100. Western Deep Levels: X 35.

(Photomicrographs by M. Seda.)

GOLD RECOVERY PI

Reference to the tables of the mineralogical data in most cases almost all gold in the minus 600 μm fraction of the plant feed and the circulating circuit materials is recovered. Furthermore, the gold is recovered preferentially: altered gold occurs in the concentrate constituting only, say, 10 per cent of the feed, it represents 50 per cent of the total gold. These gold grains display the

○ Gold
⊕ Tramp Iron



Sympathetic relationship

DESCRIPTION OF SAMPLES

Sample No.

Designation

- Nos. 1 and 2 shaft sludge
- No. 3 shaft sludge
- Rake classifier overflow
- Rake classifier return
- Washing plant cyclone
- Washing plant underflow



Photomicrograph 5
A rusted grain of tramp iron surrounded by grains of pyrite and quartz (dark grey). Western Holdings Gold Mine. Belt feed. X 600.

Photomicrograph 6
A scale. The mineral grains (pyrite, gold and quartz) are held together by hydrated iron. The ratio of gold to pyrite (both dark) is shown on the photomicrograph. Western Holdings Gold Mine. Belt feed. X 600.

Photomicrographs by M. Seda.)

GOLD RECOVERY PLANT

Reference to the tables summarizing the mineralogical data reveals that in most cases almost all of the gold in the minus 600 μ m fractions of the plant feed and the other pre-milling circuit materials is already liberated. Furthermore, the gold is liberated preferentially: although the liberated gold occurs in a fraction constituting only, say, 10 to 20 per cent of the feed, it represents some 50 per cent of the total gold content. These gold grains display their natural

shapes, and very few show signs of mechanical distortion. All of the grains are tarnished.

After ball-milling, 90 per cent and more of the gold is usually liberated as free, tarnished grains frequently showing evidence of flattening and distortion. (See photomicrographs 2 and 3, Plate I.) Even if part of the tarnish of an occasional gold particle is momentarily scraped off, it is immediately replaced. Secondly, during ball-milling, copious quantities of finely divided tramp iron are

produced — sometimes as much as one kg per ton of ore milled, i.e. an amount 50 times higher than the amount of gold in the ore. From here onwards, the tramp iron plays its deleterious role in the circuit.

Examination of polished sections reveals that much of the tramp iron is heavily oxidized, the grains becoming surrounded by a thick crust of hydrated oxide. Tramp iron that has been circulating in the plant for some time may be completely rusted away, or only a small remnant of the

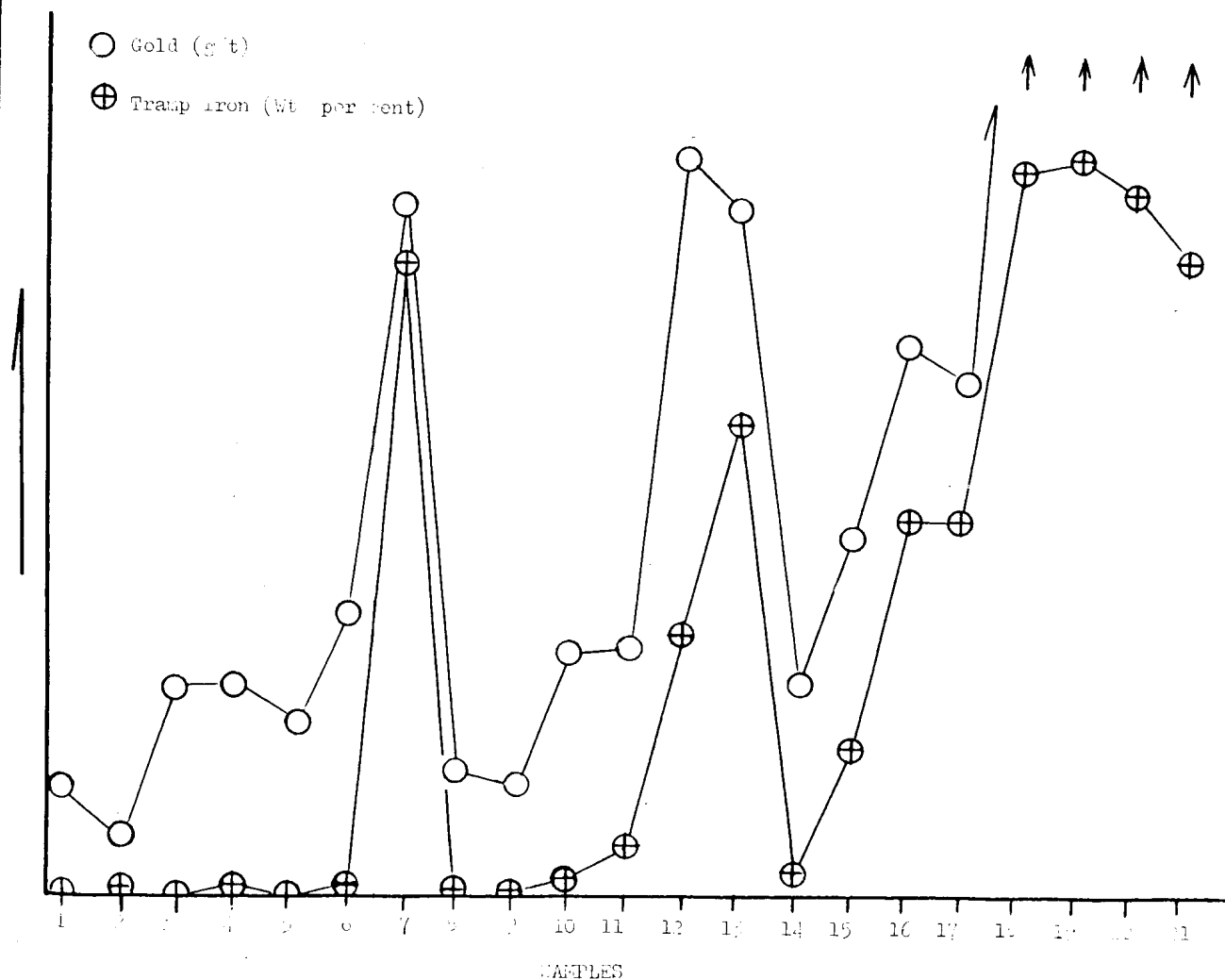


FIGURE 1

Sympathetic relationship between the abundance of gold and tramp iron in a suite of samples from Western Holdings Gold Mine.

DESCRIPTION OF SAMPLES

Sample No.	Designation
1.	Nos. 1 and 2 shaft sludge
2.	No. 3 shaft sludge
3.	Rake classifier O/flow
4.	Rake classifier return
5.	Washing plant cyclone O/flow
6.	Washing plant U/flow

7.	Dewatering cyclone U/flow
8.	Ball mill feed
9.	Ball mill cyclone O/flow
10.	Secondary tube outlet
11.	Secondary cyclone U/flow
12.	Kreb tertiary cyclone U/flow
13.	Tertiary tube outlet
14.	Tertiary cyclone O/flow
15.	Spargo tertiary cyclone U/flow

16.	Johnson concentrator tails, nos. 1 and 2 banks
17.	Johnson concentrator tails, no. 3 bank
18.	Feed to cleaner tables, nos. 1 and 2 banks
19.	Feed to cleaner table, no. 3 bank
20.	Cleaner table tailings, nos. 1 and 2 banks
21.	Cleaner table tailings, no. 3 bank

original metallic iron may remain in the core of the pseudomorph of alteration products. (See photomicrograph 5, Plate II.)

Unfortunately, the particles of free gold and tramp iron have by now acquired very similar properties: both are covered by hydrated iron oxide, and both are of high specific gravity. It is not surprising, therefore, that the free gold and tramp iron show a similar concentration behaviour during passage through the plant. This relationship is illustrated in Fig. 1, which reveals that, by and large, the relative abundance of gold and tramp iron fluctuates sympathetically from sample to sample.

One unfortunate aspect of the similar concentration behaviour of the gold and tramp iron is the very real possibility that a proportion of the gold may literally be "crowded out" of a concentration circuit by the superabundant tramp iron. A second result of the tendency of these two constituents to concentrate together is that the iron, which is in a state of rapid oxidation, is strategically placed to contribute to the coating of the gold particles, and to cause the formation of firmly cemented aggregates of gold and other heavy-mineral constituents. The common nature of the coatings on gold and tramp iron most probably assists substantially in joining the particles together.

Examples of mineral aggregates cemented by hydrated iron oxide are common. Possibly the most significant is the scale deposited on the concrete walls of sumps and launders, and on the walls of cyclones and, presumably, other equipment. In photomicrograph 6, Plate II, a cross section of gold-bearing scale from a sump at Western Deep Levels is shown. Strangely, gold seems to be preferentially attracted to such scales, which may assay several kg per tonne of total precious metals.

It is also interesting that the aggregates cemented with hydrated iron oxide must be capable of forming very rapidly, as evidenced by the build-up of a thick deposit of gold-rich scale on the walls of the cyclone used to fill the amalgam barrel at Western Deep Levels. The gold and other mineral grains show a distinct

preferred orientation, and are arranged in cyclic layers, thus indicating formation of the scale during operation of the cyclone.

At this juncture, mention should also be made of the deleterious effects of stockpiling ore for any length of time. As one could imagine, the coating on the gold grains soon becomes so pronounced that prior treatment is needed before efficient gold recovery is possible. Bleeding the untreated material into the recovery circuit invariably leads to noticeable increases in the residue values.

The same problem, only in an intensified form, applies to the recovery of gold from old dumps. In such dumps, the sulphides are in a process of decomposition (see photomicrograph 1, Plate II), thus providing copious additional quantities of secondary iron colloids, firmly cementing aggregates of mineral fragments (including gold), and heavily encrusting free gold (see photomicrographs 4 and 6, Plate II). Photomicrographs 2 and 3, Plate II illustrate the deposits of nodular, hydrated iron oxide formed typically in this environment.

In the gold recovery plant, the overflow and underflow figures relating to the various cyclones (see Tables I to IV) reveal the interesting fact that the grain size of the gold in the overflow fraction is consistently very similar to that in the underflow, and, which is more important, reveal that in both fractions the proportion of locked gold is almost negligible. The comparatively coarse grain size of the gold in the overflow fraction is most probably due to the flattish shape of the grains. Thucholite also collects in the overflow, and is sent from here, via the cyanidation plant, to the residue dump. Recycling any of the cyclone products for remilling seems to serve no useful purpose, but could result in further deformation of the gold particles and their contamination by mineral matter pressed into them. These mutilated grains reporting in the tertiary cyclone underflow eventually collect in the concentrator tailings and are almost invariably returned for yet another dose of milling. The circulating load thus created can only result in the loss of gold particles that have lost

all of their original properties. Very obviously, it would be beneficial rather to remove the gold from the circuit as soon as it is liberated.

It testifies to the efficiency of the current cyanidation and amalgamation processes that such a high proportion of the tarnished, milled gold grains is still being recovered. The tarnish is probably of a porous nature. In a successful attempt at increasing the recovery efficiencies, concentrates were treated with hydrochloric acid to reduce the effect of the iron oxide coating. This treatment has, for example, contributed to the remarkable amalgamation efficiencies (99.46 per cent) achieved by Western Deep Levels.

The gold in amalgam-barrel residues consists essentially of free tarnished or incompletely amalgamated grains (see photomicrograph 4, Plate I), and the current practice at some mines of recycling these to the milling circuit can only result in gold losses.

The locked gold in amalgam-barrel residues constitutes a minor proportion of the total gold. Most of this gold occurs as minute specks (less than 10 microns in size) and veinlets in uraninite. Gold occlusions also occur in sulphide, skutterudite silicate minerals, hydrated iron oxides, titanium compounds, and a variety of other minerals. In all of these, the gold occlusions are so minute that no amount of additional milling will ensure their complete liberation. We shall now consider the mechanism of the development of hydrated iron oxide tarnish on the gold grains.

THE NATURE AND ORIGIN OF THE COATING ON GOLD

By means of the electron microscope, sectioned Witwatersrand gold grains in unprocessed Carbon Leader Basal and Vaal Reefs were found to contain a more or less constant few per cent of silver, together with traces of copper and nickel.

The samples of ore were crushed to fragments approximately one inch in diameter, thereby providing fresh exposures of gold grains for examination. The surface of fragments selected for examination were cleared in an ultrasonic cleaner bath using acetone, alcohol, and methyl ethyl ketone successively. The spec-

original properties. It would be beneficial to remove the gold from as soon as it is liberated.

ies to the efficiency of cyanidation and amalgamation processes that such a removal of the tarnished gold grains is still being investigated. The tarnish is probably a surface film. In a successful test, increasing the recovery of concentrates were treated with hydrochloric acid to remove the iron oxide coating. This treatment has, for example, led to the remarkable amalgamation efficiencies (99.46 per cent) by Western Deep Levels. Gold in amalgam-barrel residues consists essentially of free or incompletely amalgamated grains (see photomicrograph), and the current practice of recycling these residues can only result in losses.

Unrecovered gold in amalgam residues constitutes a minor portion of the total gold. Most of it occurs as minute specks (10 microns in size) and is associated with uraninite. Gold inclusions in sulphide, skutterudite minerals, hydrated iron oxides, uranium compounds, and other minerals. In all cases, the gold inclusions are so small that no amount of additional treatment will ensure their complete recovery.

We shall now consider the mechanism of the development of iron oxide tarnish on the

TEXTURE AND ORIGIN OF COATING ON GOLD

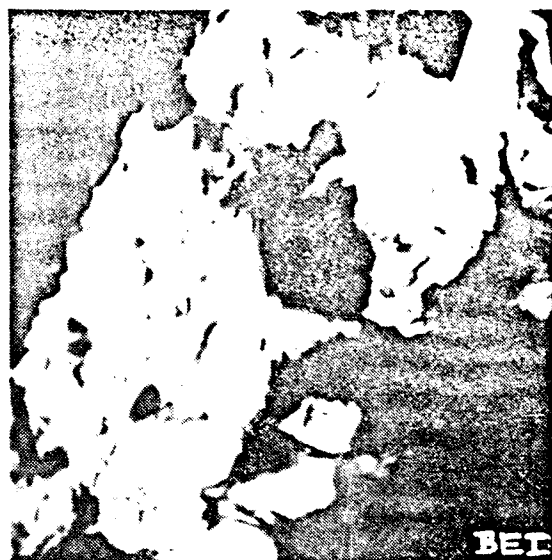
Results of the electron microprobe analysis of Witwatersrand gold, unprocessed Carbon Leader, and Vaal Reefs were found to show a more or less constant amount of silver, together with copper and nickel.

Samples of ore were crushed to approximately one inch, thereby providing fresh surfaces of gold grains for examination. The surface of fragments for examination were cleaned in ultrasonic cleaner bath, one, alcohol, and methanol successively. The specimen

MINING AND METALLURGY



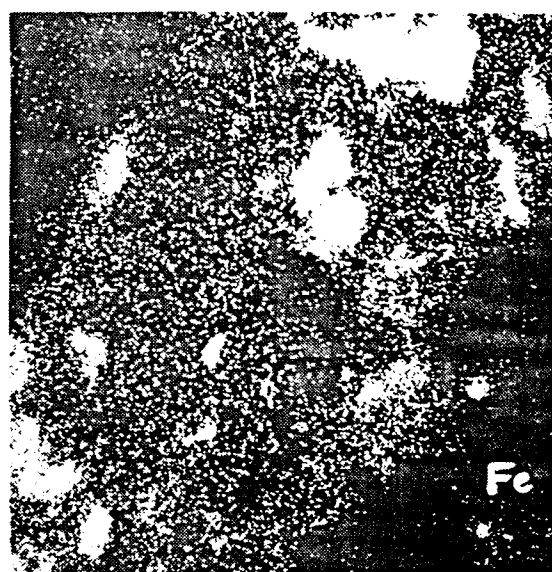
X 600
SEI



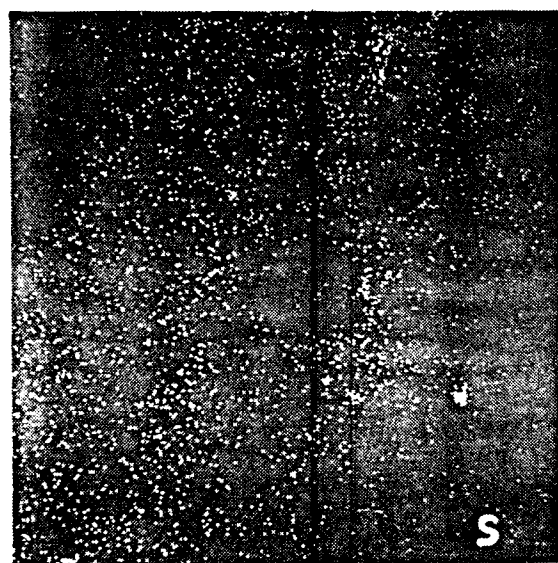
BEI



Au



Fe



S

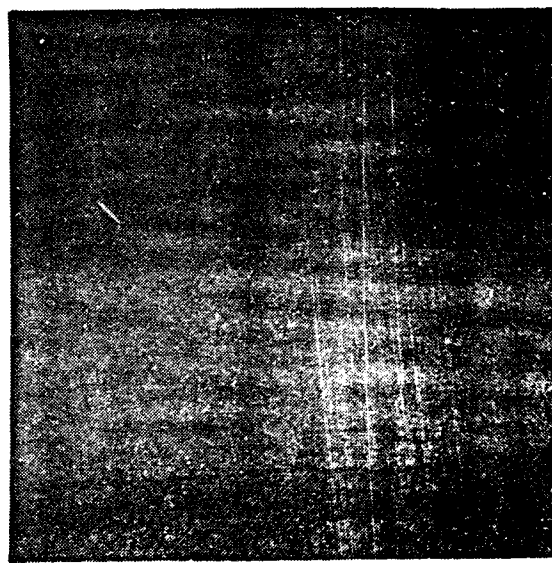


PLATE III

1	2
3	4
5	

Figures

Linear magnification: X 600
Scale: 10 microns = 6 mm.

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Electron Microprobe CRT Images

Figure 1

Secondary electron image of a gold grain in Basal Reef, showing delicate surface textures giving rise to a large surface area. The grain is coated with a very thin layer of iron sulphide.

Figure 2

Compositional back-scattered electron image of the same area.

Figure 3

Distribution of gold.

Figure 4

Distribution of iron, in the surface coating and in iron oxide crystals attached to the surface of the gold grain.

Figure 5

Distribution of sulphur (in the surface coating).

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mens were thereafter flash-coated with a conductive layer of pure carbon and examined in the electron microprobe.

Without exception, the outer surfaces of the gold grains examined were found to possess a thin layer of iron sulphide or iron oxide (Plate III) or both. Where the sulphide coating was thicker than average, the iron and sulphur were found to be present in constant proportions, probably as pyrrhotite or pyrite.

On some grains the alloy was seen to be coated so thickly with iron oxide as to be almost completely concealed from detection by the microprobe. It is likely that many grains were so thickly coated as to have escaped detection altogether.

Where gold-alloy grains were found in the proximity of zinc sulphide (sphalerite), the surface coating on the alloy grains was found to contain zinc in addition to sulphur and iron. Lead sulphide may coat the alloy grains when galena is abundant and in close proximity to the alloy grains.

Laboratory experiments were carried out with pure gold, pure silver, and gold/silver alloy concentrated from the Witwatersrand Reefs. The metals were treated with Fe^{2+} , S^{2-} , H^+ , and SO_4^{2-} ions in dilute aqueous solution at 40°C .

After twelve hours the silver was heavily coated with a layer of silver sulphide containing minor concentrations of iron, the pure gold had not reacted at all, and a readily detectable sulphide coating formed on the gold/silver alloy.

It thus appears that the silver in solution in the alloy becomes available for reaction with sulphide ions in solution, thereby forming a silver sulphide surface deposit.

HYPOTHESIS FOR THE FORMATION OF REFRACTORY COATED GOLD IN WITWATERSRAND GOLD ORE

Studies of the conglomerate reefs of the Witwatersrand have indicated that the age of the system is in the region of 2 600 million years. There is abundant evidence that, during the vast expanse of time following its formation, it has been subjected to metamorphic processes; and it may be concluded that, at

least during the metamorphic history of the reef, free sulphide ions were available, and sulphides were formed readily.

In the laboratory experiments described earlier, it was demonstrated that silver-bearing gold is easily attacked by sulphide ions, whereas pure gold is inert. It is concluded that similar reactions have taken place in the reefs.

The hypothesis advanced is that, in nature, silver atoms in the peripheral regions of gold/silver alloy grains are able to combine with the available sulphur. Once sulphur atoms have been bonded to the alloy surface by this means, the alloy grains become excellent seeds for the growth of yet more sulphide, especially iron sulphides. To at least some extent such coatings have been observed on all the Witwatersrand gold grains studied.

By subsequent oxidation, the iron sulphide coatings have become capable of seeding further growth of iron oxides. In the course of mining and plant operations, the process initiated in nature can be continued with extraordinary rapidity owing to the abundance of introduced metallic iron and the prevailing highly oxidizing conditions.

The chemical and galvanic decomposition of tramp iron and the precipitation of ferric hydroxides in the alkaline milling and processing circuits are readily observable. In a similar manner the introduction of calcium into the surface coatings, by the addition of calcium hydroxide to the pulp, has also been demonstrated.

It is interesting also to note that dilute nitric acid is found to be better than dilute hydrochloric acid for removing the coating from the gold/silver alloy prior to mercury amalgamation on the gold plants. Silver in the surface of the alloy grains will react with the acids, and with hydrochloric acid only, forms a very thin coating of insoluble silver chloride on the surface of the alloy grains. With nitric acid, no tarnish forms.

Coated gold, and its adverse effects in plant operations, was known in the U.S.A. as early as 1934¹. Head² states, "These coatings may encase the gold particles entirely, or they

may exist as films or tarnishes whose presence is rendered perceptible only by comparison with normal clean gold". Using microchemical tests, he established that iron was the essential constituent of the coatings, but offered no explanation for its presence. He observed the coated gold was prevalent in pyrite deposits, and noted that the coating renders the gold refractory to amalgamation and other recovery processes.

As early as 1889, reference was made to "rebellious gold" that "resists recovery"³, but this property was not specifically correlated with the presence of an iron oxide coating. Even earlier, Stetefeldt⁴ came very close to the truth when he spoke of refractory gold as "rusty gold".

CONCLUSIONS

Great benefit should result from removing the gold from the circuit as soon as it is liberated. Not only unnecessary milling a wasteful operation, but it contributes substantially to gold losses.

Tramp iron is a most deleterious constituent in the plant circuit. It results in the formation of copious quantities of colloidal iron compounds, which add to the hydrate-iron oxide coating on individual gold grains, and contributes to the formation of rusty mineral aggregate. As a result of the iron oxide coatings and encrustations, gold recovery becomes more difficult and occasionally, impossible.

Removal of tramp iron from the circuit (and separate treatment to recover entrained gold) should clearly have a beneficial effect on gold recoveries in general.

ACKNOWLEDGEMENTS

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- (ii) the size by stones, and
- (iii) the revenue secondary value per latter concept size and it is are of average

By suitable combination to arrive at the

A Mining Director and Administration, University

This paper will be published in the International Symposium on Methods in the Mineral Industry.